

## Utilization of BSA optimized cascade controller in a renewable energy-based AGC systems

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### Article Info

#### Article history:

Received May 7, 2025

Revised Dec 21, 2025

Accepted Mar 12, 2026

#### Keywords:

Automatic generation control

Automatic voltage regulation

Bird swarm algorithm

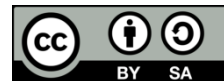
PID-TID controller

Wind turbine systems

### ABSTRACT

A novel cascade controller named proportional integral derivative-tilt integral derivative (PID-TID) is proposed for a two-area thermal-wind automatic generation control (AGC) system and its gains are optimized by a novel metaheuristic bird swarm algorithm (BSA). The BSA tuned PID-TID controller enhances dynamics over PID and TID controller in terms of settling time and peak shoots. Moreover, dynamics with wind integration have shown significant improvement over thermal system alone. Further system has shown enhanced dynamics with redox flow batteries (RFB) over thermal-wind system. Furthermore, studies with automatic voltage regulation (AVR) strengthen voltage stability. Also, responses with PID-TID have shown steady dynamic profile at various loading conditions. Integrating wind energy into thermal system results in significant enhancements in dynamics showcasing greater stability. Also, improvements are evident with the RFB introduction, enhance dynamic with in hybrid system. The incorporation of AVR enhance voltage stability. The proposed PID-TID demonstrates significant robustness ensuring stable response under loading condition and effectively boost dynamic performance.

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## 1. INTRODUCTION

Balancing of power has become challenge due to increase in grid's size and complexity. Also, keeping the system stable at permissible limits has become difficult. This issue can be addressed by automatic generation control (AGC) that maintains frequency, voltage and power in permissible limits [1], [2]. AGC works initiated by one area and broaden to complicated multi-area systems [3]-[5] considering nonlinearities like GDB, delay, and GRC. Further, frequency-voltage coupling exists due to interaction of AGC with automatic voltage regulator (AVR) loops [1], [2], [5]. The efficient integration of renewables including solar and wind turbine systems (WTS), is studied in AGC [6]-[8]. The study in [9], [10] examined WTS with constant wind velocity. However, because of intrinsic wind changes, WTS production is variable. The incorporation of WTS into AGC-AVR framework has not received much attention, although it reduces this intermittency.

Power system performance deteriorates under faulty conditions leading to transients worsening system dynamics. This issue can be mitigated by the energy storage device (ESD) integration [10], [11]. ESD such as redox flow battery (RFB) and its advantages in AGC studies are noted in [10]. These findings can be extended to more complex configurations, such as two-area systems, particularly when integrating renewable energy sources.

The advancement of the auxiliary controller has been the primary focus of AGC research. Basic fractional [12], cascade and tilt controllers such as proportional integral derivative (PID) [13], PI-PD [14], tilt integral derivative (TID) [15], fuzzy [16], and sliding controller [17] have been introduced over time. However, a novel combination such as PID-TID for two-area AGC-AVR with RS has not been investigated.

Recent developments in AGC research have shown that many metaheuristic methods are successfully applied, such as swarm [15], crow search [18], hybrid crow search [19], genetic [20], antlion [21], and cuckoo search [22]. Meng *et al.* [23] introduced an optimization technique known as the BSA, inspired by the cooperative foraging behavior of birds. The algorithm effectively achieves global optimization with fewer iterations, offering high accuracy and fast convergence. Also, BSA has significantly improved dynamics of AGC systems [24], [25]. Yet the impact of BSA on AGC-AVR is to be evaluated.

Sensitivity analysis is commonly employed in AGC to evaluate the controller robustness against substantial load oscillations in the system [19], [25]. While this work introduces a novel controller, termed TIDN, a sensitivity analysis has yet to be performed. This presents an opportunity for further research. The following objectives have been outlined and are: i) to develop a two-area AGC system incorporating thermal, WTS components; ii) implement several controllers like TID, PID, and cascaded of PID and TID (PID-TID), in system model (Figure 1); iii) employing BSA for concurrent optimization; iv) assessment of system dynamics due to WTS integration; v) evaluation of system dynamic performance with ESD integration; vi) sensitivity-based robustness assessment, and vii) to study the impact of AVR loop on WTS-thermal-ESD system.

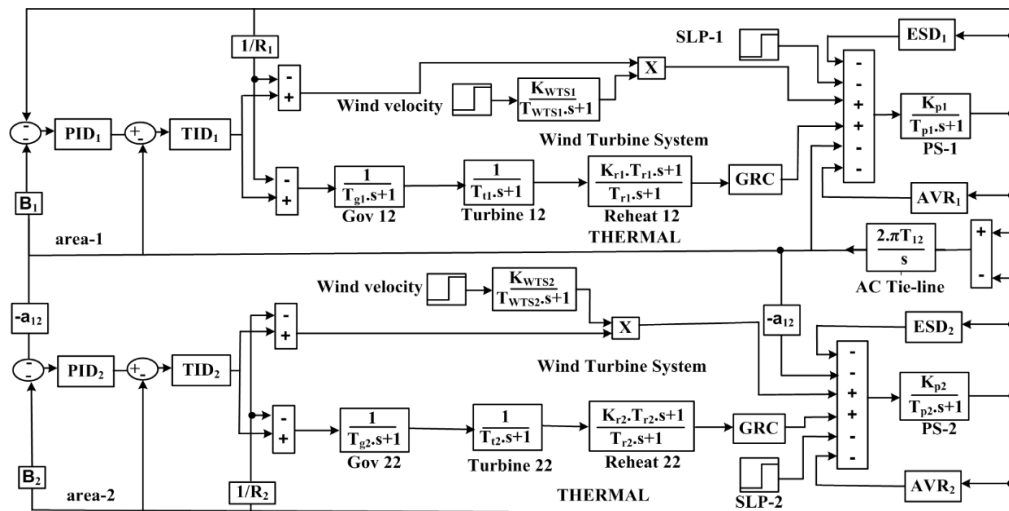


Figure 1. Proposed system model

## 2. SYSTEM DESCRIPTION

### 2.1. Proposed controller

An innovative controller that combines both integer and fractional controllers is the tilt controller, first introduced in [6]. While the structures of PID and TID controllers are similar, the TID controller introduces a scaling factor of 1/sn to the proportional term of the PID. However, incorporating derivative control within the forward path can lead to the undesired phenomenon of derivative kick in electronic systems [6]. The cascading PID and TID controllers provide fast and stable frequency regulation. PID handles rapid deviations, while TID addresses slower disturbances, together improving stability, reducing overshoot, and enhancing overall system performance. The equations of PID, PID, and the cascaded PID-TID are in (1)-(3) respectively.

$$F_1(s) = K_{KPi} + \frac{K_{KLi}}{s} + K_{KDi}s \tag{1}$$

$$F_2(s) = \frac{K_{KTi}}{1/s^{nKi}} + \frac{K_{KLi}}{s} + K_{KDi}s \tag{2}$$

$$F_{PID-TID}(s) = F_1(s) + F_2(s) \tag{3}$$

**2.2. Bird swarm algorithm**

Meng *et al.* [23] proposed a swarm intelligence algorithm with bird flock behavior named BSA. The algorithm models the intelligence of birds based on key behaviors such as foraging, flying, and maintaining alertness. BSA primarily simulates bird movements through three strategies: i) searching for food, ii) staying alert in response to potential threats, and iii) escaping from predators. Foraging behavior in BSA is represented in (4), where birds move toward their personal best and the global best positions to exploit promising solutions.

$$X_{p,q}^{i+1} = X_{p,q}^i + (P_{p,q} - X_{p,q}^m) \times D \times rand_j(0,1) + (g_p - X_{p,q}^i) \times t \times rand_j(0,1) \tag{4}$$

Where position (x), dimension (q), birds count (p), past position (PP), random (rand), social (t), and cognitive (P) coefficients. Flight behavior in (5) and (6) uses flight lengths (fl = 0–2) and alternating roles to explore new regions of the search space.

$$X_{p,q}^{i+1} = X_{p,q}^i + A_1(mean_q - X_{p,q}^m) \times rand_i(0,1) + A_2(P_{p,q} - X_{p,q}^m) \times rand_i(-1,1) \tag{5}$$

$$X_{p,q}^{j+1} = X_{p,q}^n + randn_i(0,1) \times X_{p,q}^j \tag{6}$$

Vigilance behavior in (7) describes how birds at the swarm’s edge stay alert to reduce predator risk. It flowchart is in Figure 2.

$$X_{p,q}^{i+1} = X_{p,q}^j + (X_{p,q}^j - X_{p,q}^j) \times fl \times rand_i(0,1) \tag{7}$$

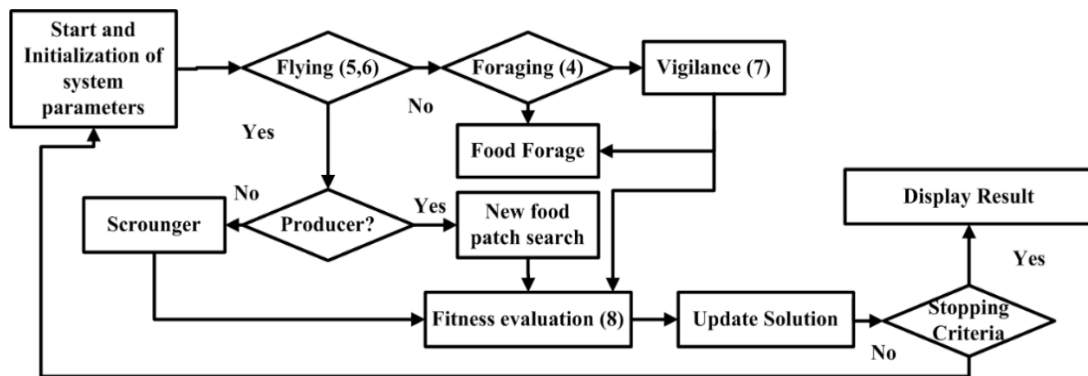


Figure 2. BSA working diagram

**3. INVESTIGATED SYSTEM**

The transfer function model of a two-area thermal system is integrated with a WTS, is in Figure 1. The system's nominal parameters, derived from references [8], [20], are detailed in the appendix. The WTS, RFB, and AVR loops are simplified into low-order linear models. WTS has a rigid rotor with power responding linearly to frequency changes, assuming nearly constant wind. RFB uses linear governor and turbine dynamics with reheat delay, ignoring nonlinearities. System dynamics are analyzed by using PID, TID, and PID-TID controller in a thermal-wind-RFB-AVR system. Controller gains are optimized by BSA technique considering ISE as performance index in (8).

$$\eta_{ISE} = \int_0^t \{(\Delta F_m)^2 + (\Delta P_{m-n})^2\} dt \tag{8}$$

Nominal values are: WTS:  $K_{WTS} = 1.25$ ,  $T_{WTS} = 0.041$  s; Thermal system:  $F_i = 60$  Hz,  $B_i = 0.425$  MW p.u.,  $H_i = 5.00$  s,  $T_{ij} = 0.0860$  p.u. MW/rad,  $T_{gi} = 0.080$  s,  $K_{pi} = 120$  Hz/p.u.,  $R_i = 2.4$  Hz/p.u.,  $B_i = 0.425$  MW/Hz,  $T_{pi} = 20$  s,  $T_{ti} = 0.3$  s,  $K_{ri} = 0.5$ ,  $T_{ri} = 10$  s; and RFB as ESD:  $K_{RFB} = 1.0$ ,  $T_{RFB} = 0.01$  s.

**4. ANALYSIS OF SIMULATION RESULTS**

**4.1. Controllers’ assessment**

Thermal system in Figure 1 is studied with PID, TID, and PID-TID controllers independently. The gains of these controllers are enhanced by BSA, with the optimal values provided in Table 1. Comparison of

the controller dynamics is shown in Figure 3(a). Table 2 summarizes the performance indicators, including POS, PUS, and ST, which are derived from the results depicted in Figure 3(a).

A comprehensive examination of Figure 3(a), along with the performance metrics in Table 2, indicates the PID-TID controller demonstrates superior dynamics over the PID and TID controllers and is utilized for the remainder of the studies. The PID-TID controller was tuned using BSA with different performance indices, and Figure 3(b) shows that ISE yields the best improvement in system dynamics.

Table 1. Optimum PID, TID, and PID-TID controller values

Controller	Optimal values
PID	$K_{KPI}^* = 0.5300, K_{KI1}^* = 0.2090, K_{KD1}^* = 0.2402, K_{KP2}^* = 0.6004, K_{KI2}^* = 0.2087, K_{KD2}^* = 0.2140$
TID	$K_{KTI}^* = 0.730, K_{KI1}^* = 0.3021, K_{KD1}^* = 0.2450, N_{K1}^* = 92.520, n_{K1} = 4.420, K_{KT2}^* = 0.7341, K_{KI2}^* = 0.2940, K_{KD2}^* = 0.2501, N_{K2}^* = 92.620, n_{K2} = 4.360$
PID-TID	$K_{KPI}^* = 0.6600, K_{KI1}^* = 0.2090, K_{KD1}^* = 0.2342, K_{KP2}^* = 0.5990, K_{KI2}^* = 0.2072, K_{KD2}^* = 0.2391, K_{KTI}^* = 0.683, K_{KI1}^* = 0.2730, K_{KD1}^* = 0.2105, n_{K1} = 4.600, K_{KT2}^* = 0.6180, K_{KI2}^* = 0.2050, K_{KD2}^* = 0.2016, n_{K2} = 4.601$

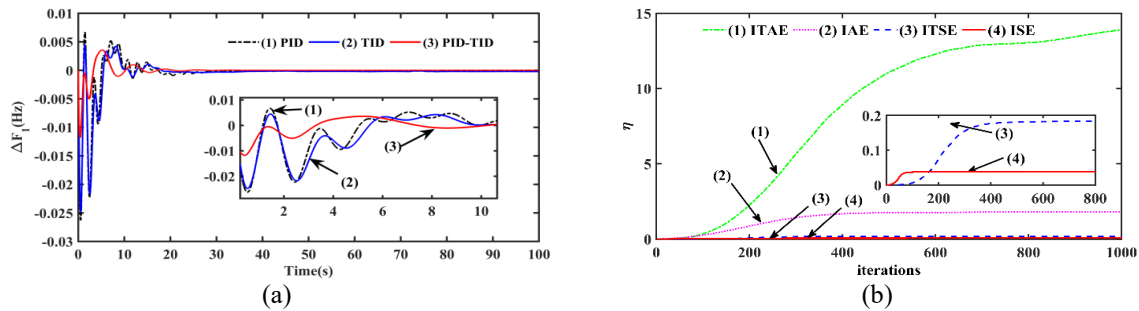


Figure 3. Performance comparison of control strategies: (a) for PI, PID, and PID–TID controller comparisons and (b) comparisons with various indices

Table 2. System dynamic performance comparison from Figure 3

Responses	Indices	PID-TID	PID	PI
$\Delta F_1$	POs	0.0035	0.0044	0.0067
	PUs	0.0116	0.0247	0.0260
	ST	37.990	46.860	53.700

4.2. Comparison with various algorithms

Various algorithms such as BSA, flower pollination algorithm and cuckoo search are considered with metrics such as convergence rate are evaluated. Figure 4(a) shows the simulation results for the three algorithms, with convergence analysis confirming the BSA algorithm’s superiority in optimizing the PID-TID controller. The results demonstrate BSA’s potential to enhance convergence rate and accuracy in power system optimization.

4.3. Evaluation of WTS integration impact on system performance

In Case-4.1, the system under investigation is amalgamated with WTS. The PID-TID controller, identified as the best performer in Case-4.1, is employed and is optimized by BSA. The optimal PID-TID parameters are in Table 3. The dynamic comparison is made with the thermal unit in Figure 4(b). It clearly indicates that the integration of WTS leads to enhanced dynamic performance.

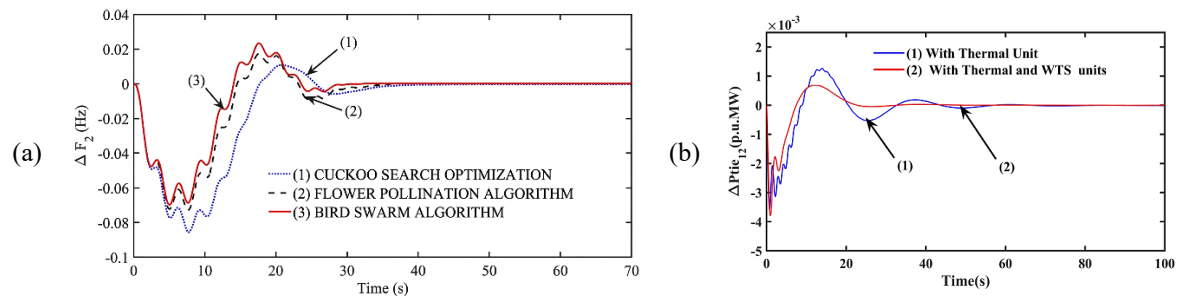


Figure 4. Dynamic comparisons: (a) algorithm comparisons and (b) with and without WTS units

Table 3. Optimum values of the PID-TID controller considering WTS unit

Parameter	Value	Parameter	Value	Parameter	Value
$K_{KP1}^*$	0.6800	$K_{KI1}^*$	0.2205	$K_{KD1}^*$	0.2472
$K_{KP2}^*$	0.6200	$K_{KI2}^*$	0.2088	$K_{KD2}^*$	0.2410
$K_{KT1}^*$	0.6895	$n_{K11}^*$	0.3001	$n_{K12}^*$	0.2178
$n_{K1}^*$	4.580	$K_{KT2}^*$	0.6310	$n_{K2}^*$	0.2086
$K_{KD2}^*$	0.2210	$n_{K2}^*$	4.001		

**4.4. Evaluation of ESD integration on system dynamics**

Section 4.3 explores the integration of RFB into the system, considering the PID-TID controller adjusted by BSA, with the optimal values in Table 4. The dynamics with and without ESD are illustrated in Figure 5. From Figures 5(a) and 5(b), the system with the ESD link exhibits significantly better dynamic performance compared to the system without it.

Table 4. Optimal PID-TID controller with ESD

Parameter	Value	Parameter	Value	Parameter	Value
$K_{KP1}^*$	0.6905	$K_{KI1}^*$	0.2278	$K_{KD1}^*$	0.2494
$K_{KP2}^*$	0.6507	$K_{KI2}^*$	0.2280	$K_{KD2}^*$	0.2500
$K_{KT1}^*$	0.7070	$n_{K11}^*$	0.3100	$n_{K12}^*$	0.2202
$n_{K1}^*$	5.002	$K_{KT2}^*$	0.6440	$n_{K2}^*$	0.2100
$K_{KD2}^*$	0.2415	$n_{K2}^*$	5.300		

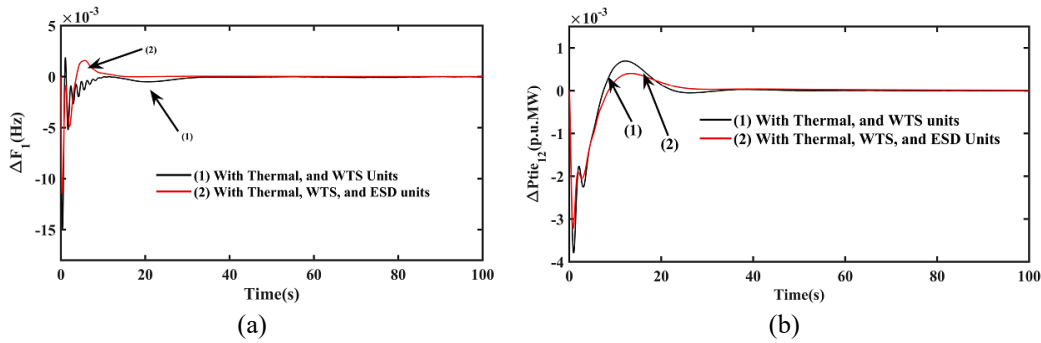


Figure 5. System performance with and without ESD integration: (a)  $\Delta F_1$  and (b)  $\Delta P_{tie12}$

**4.5. Sensitivity analysis**

To estimate the sturdiness of the top-performing PID-TID controller from Case Study-A, we consider two loading scenarios—25% and 75%—by varying the system load by  $\pm 25\%$  from the nominal 50% loading. After applying BSA, the optimal controller settings for each scenario are presented in Table 5. Figures 6(a) and 6(b) compare and illustrate the system dynamics for three load scenarios: 25%, 50%, and 75%. The PID-TID controller consistently maintains strong performance, even with load deviations of  $\pm 25\%$  from the nominal value, as shown by the dynamic responses. This demonstrates that the PID-TID controller offers stable performance across a range of system loading conditions.

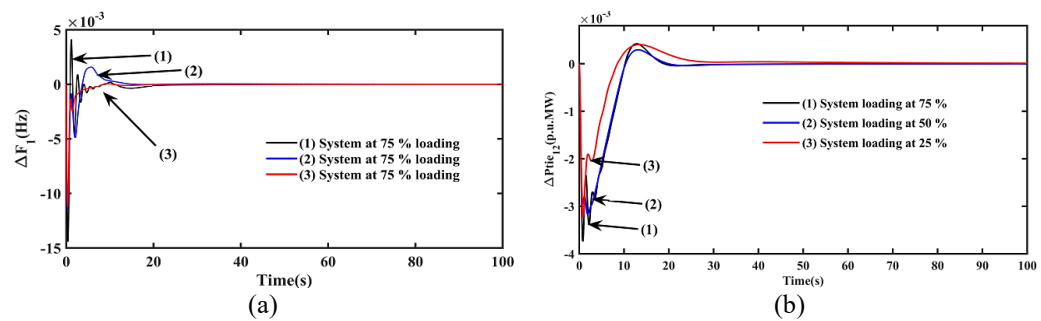


Figure 6. System performance at different loading: (a)  $\Delta F_1$  and (b)  $\Delta P_{tie1-2}$

**4.6. Impact of AVR loop on WTS-thermal-ESD system**

Figure 1 with RFB-WTS-thermal is integrated with AVR and is under study. A thermal power plant, wind unit, RFB, and AVR loop are considered. BSA optimized the PID-TID gains, plotting their responses in Figure 7. The responses in Figures 7(a) and 7(b) suggest the AVR loop outcomes over AGC system by enhancing voltage and frequency stability.

Table 5. Control settings of PID-TID at varied loading

Loading	Parameter	Value	Parameter	Value	Parameter	Value
At 25 %	$K_{KP1}^*$	0.6250	$K_{KI1}^*$	0.1990	$K_{KD1}^*$	0.2020
	$K_{KP2}^*$	0.5900	$K_{KI2}^*$	0.1990	$K_{KD2}^*$	0.2210
	$K_{KT1}^*$	0.6350	$K_{KI1}^*$	0.2605	$K_{KD1}^*$	0.2000
	$\eta_{K1}^*$	3.9900	$K_{KT2}^*$	0.6050	$K_{KI2}^*$	0.2000
	$K_{KD2}^*$	0.2011	$\eta_{K2}^*$	4.000		
At 75 %	$K_{KP1}^*$	0.6850	$K_{KI1}^*$	0.2500	$K_{KD1}^*$	0.2402
	$K_{KP2}^*$	0.6000	$K_{KI2}^*$	0.2326	$K_{KD2}^*$	0.2498
	$K_{KT1}^*$	0.6550	$K_{KI1}^*$	0.2860	$K_{KD1}^*$	0.2200
	$\eta_{K1}^*$	4.850	$K_{KT2}^*$	0.6550	$K_{KI2}^*$	0.2230
	$K_{KD2}^*$	0.2210	$\eta_{K2}^*$	4.500		

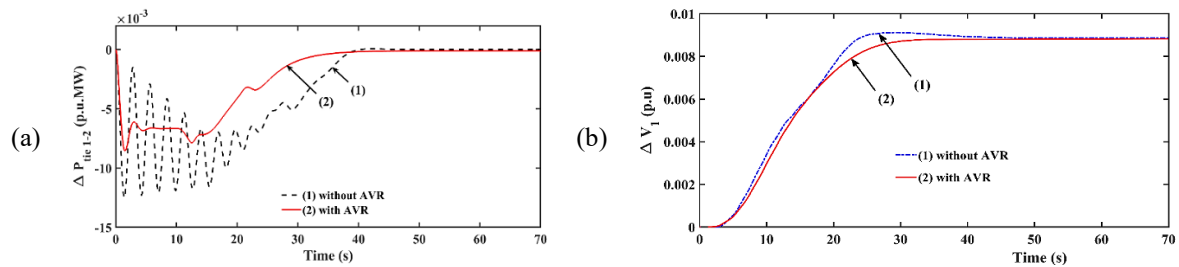


Figure 7. Impact of AVR: (a)  $\Delta P_{tie1-2}$  and (b)  $\Delta V_1$

**5. CONCLUSION**

An effort was made to improve the recital of a two-area AGC system by employing various secondary controllers, including PID-TID, PID, and TID controllers. The characteristics of these tilt controllers were optimized using the BSA. The results indicated that the PID-TID controller outperforms over others when comparing the dynamics. The integration of Wind units enhanced the dynamics of the two-area thermal system compared to a system without renewable sources. Additionally, the inclusion of a redox batteries further improved system performance. The sensitivity study confirmed that the PID-TID controller maintains stable performance across a broad range of system loading scenarios, eliminating the need to modify the original parameter values. Furthermore, studies with AVR have shown significant improvement in system dynamics. Future directions include hardware-in-the-loop testing, extending to hybrid renewable systems, and comparing performance with other metaheuristic optimization algorithms.

**FUNDING INFORMATION**

No funding involved.

**AUTHOR CONTRIBUTIONS STATEMENT**

This journal uses the Contributor Roles Taxonomy (CRediT) to recognize individual author contributions, reduce authorship disputes, and facilitate collaboration.

Name of Author	C	M	So	Va	Fo	I	R	D	O	E	Vi	Su	P	Fu
Rambabu Kasukurthi	✓	✓	✓	✓	✓	✓		✓	✓	✓				✓
R. Srinu Naik		✓				✓		✓	✓	✓	✓	✓		

- C : Conceptualization
- M : Methodology
- So : Software
- Va : Validation
- Fo : Formal analysis
- I : Investigation
- R : Resources
- D : Data Curation
- O : Writing - Original Draft
- E : Writing - Review & Editing
- Vi : Visualization
- Su : Supervision
- P : Project administration
- Fu : Funding acquisition

## CONFLICT OF INTEREST STATEMENT

No conflict of interest.

## INFORMED CONSENT

We have obtained informed consent from all individuals included in this study.

## ETHICAL APPROVAL

The research related to animal use has been complied with all the relevant national regulations and institutional policies for the care and use of animals.

## DATA AVAILABILITY

Data availability is not applicable to this paper as no new data were created or analyzed in this study.





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